Creep or Stick?

Spatial variations of fault friction, implications for earthquake hazard

Jean-Philippe Avouac

Collaborators

Vicky Stevens Marion Thomas Thomas Ader Ozgun Konca Laurent Bollinger Francois Ayoub Sylvain Barbot Anthony Sladen Andrew Kosistsky Mohamed Chlieh Hugo Perfettini Don Helmberger Nadia Lapusta Kerry Sieh



Talk Outline

- Interseismic coupling
- The Sumatra megathrust
- The Longitudinal Valley Fault, Taiwan
- The Himalayan megathrust
- Dynamic modeling: Parkfield, SAF
- What makes fault stick or creep?







Interseismic coupling

Definition: ISC

 χ_i =deficit of slip/long term slip

Determination:

Elastic Dislocation Modeling of Interseismic geodetic displacements





Interseismic coupling

Relation to Seismic slip:

If deformation of the hanging wall in the long term is negligible then **seismic slip and aseismic transients** must balance ISC

Implication:

The ISC pattern should determine the location, amplitude/frequency of seismic and aseismic transients.





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Dynamic Modeling





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Sources: Natawidjaja et al, (2004), Chlieh et al, (2008); Briggs et al (2006); Hsu et al (2006); Konca et al (2006, 2008)



- Interseismic coupling





- Interseismic coupling
- Mw, 8.6, 2005, Nias EQ





- Interseismic coupling
- Mw 8.6, 2005, Nias EQ
- Mw 8.4, 2007, Bengkulu EQ





- Interseismic coupling
- Mw 8.6, 2005, Nias EQ
- Mw 8.4, 2007, Bengkulu EQ
- Mw 7.9, 2007, Bengkulu EQ





Afterslip: 30% of coseismic moment release over 1 yr

- Mw 8.6, 2005, Nias EQ
- Mw 8.4, 2007, Bengkulu EQ
- Mw 7.9, 2007, Bengkulu EQ
- 1 yr afterlip following Nias EQ
- 1 yr afterlip following Bengkulu EQs





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- Interseismic coupling is highly heterogeneous
- Slip is mosty aseismic (50-60%) in the 0-40km 'Seismogenic' depth range
- Seismic ruptures seem confined to 'locked' areas. Creeping zones tend to arrest seismic ruptures.
- Afterslip increases as a logarithmic function of time.

Does the slip budget close (seismic +aseismic slip=long term slip)?

(Chlieh et al, JGR, 2008; Konca et al. 2008, Hsu et al., 2006...)











(Thomas et al, JGR, 2014; Thomas et al, Tectonophysics, 2014))



Why studying the longitudinal valley

fault?

- LVF is part of very active plate boundary
- High slip rate: > 4 cm/yr
- Aseismic creep documented at the surface



- Large earthquakes : M>7 1951 ; Mw6.8 2003
- Thrust fault: an access to exhumed fault zone





Principal Component Analysis based Inversion Method (PCAIM)

 Method based on the theory of dislocations in an elastic half space and Principal Component Applying X – USV^t Singular Value Decomposition of surface dis



PCA and theory of dislocations are linear and associative and thus you can switch their ordering.



- PCAIM can deal with any kind of time variation of fault-slip
- PCAIM can integrate simultaneously different geodetic measurement and remote sensing data.

(Kositsky and Avouac, JGR 2010, Perfettini et al, 2010)



CO-SEISMIC MODEL (2003, Mw 6.8, chengkung earthquake)







60

2008

locked zone

2008

90 cm



- Interseismic coupling is highly heterogeneous
- Slip is mosty (80%) aseismic in the 0-40km 'Seismogenic' depth range
- Seismic ruptures seem confined to 'locked' areas. Creeping zones tend to arrest seismic ruptures.

TIME EVOLUTION OF SLIP AT DEPTH



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Estimated rupture areas of major earthquakes in the Himalaya since 1700 (e.g., Ambraseys and Bilham, 2000; Hough et al, 2005).



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Seismicity follows the downdip end of Locked Fault Zone where shear stress increases in the interseismic period by > 4kPa/yr.

The moment deficit accumulates in the interseismic period at a rate of **6.6 10¹⁹ Nm/y**r.

How large and how frequent need the largest Himalaya earthquakes be?

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Estimated rupture areas of major earthquakes in the Himalaya since 1700 (e.g., Ambraseys and Bilham, 2000; Hough et al, 2005).


The Mw 2005, 7.6, Kashmir Earthquake



Surface rupture measured from cross-correlation of ASTER satellite images





The Mw 2005, 7.6, Kashmir Earthquake



Source Model



The Himalayan Megathrust



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How large and how frequent need the largest Himalaya earthquakes be?

1-Mw 7.6 : 7 yr 2- Mw 8.2 : 50 yr 3-Mw >8.5 300yr

(Ader et al., 2012)

Key points so far

- Interseismic Coupling on subduction Megathrust is highly heterogeneous./ more homogeneous on the Himalayan Megathrust
- Seismic ruptures tend to be confined within locked fault patches and to nucleate at the edges of these patches.
- The frequency/magnitude of the largest earthquakes can in principl be constrained from the determination of ISC,... but uncertainties are large.

Conceptual Model

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THE LONGITUDINAL VALLEY FAULT (TAIWAN) INSIGHTS ON FRICTIONAL PROPERTIES



 $\frac{\partial \mu_{ss}}{\partial \ln V} = a - b$



(Thomas et al., in prep)

Dynamic modeling



Dynamic modeling Modeling the Parkfield EQs Sequence on the SAF



(Barbot et al, Science, 2012)

- How to constrain frictional properties in absence of large co- and post-seismic signal?
- Why makes fault creep (or stick)?

- How to constrain frictional properties in absence of large co- and post-seismic signal?
- Why makes fault creep (or stick)?
 - Lithology a b > 0
 - Temperature
 - Water b-a

$$b-a > \lambda \frac{GD_c}{L\sigma'_n}$$





Aseismic slip dominant where T > 350°C.

consistent with laboratory experiments which show that stable frictional sliding is promoted at temperatures higher than about 300°C (for Quartzo-felspathic rocks). (Blanpied et al, 1991; Marone, 1998)

(Ader et al., 2012)



The Sumatra Megathrust



THE LONGITUDINAL VALLEY FAULT (TAIWAN)



(Thomas et al, JGR, subm.)

THE LONGITUDINAL VALLEY FAULT (TAIWAN)





- Indications that fluids promote creep:
 - Soultz-la-foret experiment (e.g., Cornet et al, 1997; Bourrouis and Bernard,2007)
 - Correlation between swarms and creeping zone (e.g., Holtkamp and Brudzinski, 2014)
 - The Brawley example (Wei et al, in prep)
 - The LSBB expriment (Guglielmi, Cappa et al, in prep)

The Brawley Swarm







In-Situ probing of fault friction from hydraulic stimulation



In-Situ probing of fault friction from hydraulic stimulation



(Guglielmi, Cappa et al., in preparation)



Comparison between measured and modelled slip on the fault (bottom) assuming rate-and-state friction (with the aging law), complete stress drop and uniform effective normal stress. Aseismic slip is induced when the ratio of the shear stress to the effective normal stress is around 0.7 (top panel). Friction parameters: μ =0.6, a=0.056, b=0.001, dc= 1 μ m.

Conclusions

- Interseismic Coupling on subduction Megathrust is highly heterogeneous.
- Seismic ruptures tend to be confined within locked fault patches and to nucleate at the edges of these patches.
- Dynamic models of the earthquake cycle can be designed and calibrated based on ISC and past seismicity. Such models might be used in the future to predict the full range of possible EQs scenario and their probability of occurrence.
- We have little understanding of the factors favoring aseismic creep and of the aseismic deformation mechanisms
- We would learn a lot from in situ probing of creeping and non creeping faults from fluid injection experiments.



Seismicity is enhanced in the winter when shortening rate across the Himalayan is increased.



Winter seismicity rate is nearly twice as large as summer seismicity rate.



(Bolllinger et al, 2007)

Horizontal displacements relative to India Note seasonal variations



Seasonal variations of surface load derived from GRACE



(Kristel Chanard)



Bettinelli et al. (2008)

Observed seasonal displacements and predictions from surface load variation





Model: Elastic response to surface load of a spherical Earth model (PREM)

(Kristel Chanard)



Bettinelli et al. (2008)

Variation of Coulomb stress due to seasonal surface loading





 Seismicity rate is approximately proportional to stress rate and no significant phase shift is observed

(Bettinelli et al, 2008)

Standard Coulomb Failure Model



Time

Assuming $\dot{S} > 0$, seismicity rate obeys:

$$R = R_0 \frac{\dot{S}}{\dot{S}_0}$$

Seismicity rate is proportional to stress rate

For periodic loading :

$$\frac{\Delta R}{R_0} = 2\pi \frac{\tau_m}{T \cdot \dot{S}_0}$$

The amplitude of seismicity rate fluctuations scale as 1/T

Standard Coulomb Failure Model Seismicity rate: $R(t) \propto \dot{\tau}(t)$ $\frac{\Delta R}{R_0} = 2\pi \frac{\tau_m}{T \cdot \dot{S}_0}$ $\tau(t) = \Delta \tau \sin^2 \pi t /_T$ **Stress:** 10^{2} 10^{1} Coulomb ΔR R_0 10⁰ 10^{-1} 10^{-2} 10^{-3} 10^{-2} 10^{-1} 10^{0} **10**¹ 10^{2} Period T

The amplitude of seismicity rate fluctuations scale as 1/T

Variation of Coulomb stress



Periodicities of Himalayan Seismicity





No correlation with tides // **Annual correlation** The absence of a detectable correlation with earth tides shows that rupture is a time-dependent process at the 12h scale (ta>12h)

12 h << nucleation time << 1yr

Standard Coulomb Failure Model Seismicity rate: $R(t) \propto \dot{\tau}(t)$ $\frac{\Delta R}{R_0} = 2\pi \frac{\tau_m}{T \cdot \dot{S}_0}$ $\tau(t) = \Delta \tau \sin^2 \pi t /_T$ **Stress:** 10^{2} 10^{1} Coulomb ΔR $\overline{R_0}$ 10⁰ Monsoor Tides 10^{-1} 10^{-2} 10^{-3} 10^{-2} 10^{-1} 10^{0} 10^{1} 10^{2} Period T

Failure has to be a time-dependent process
Rate&State Friction Model



$$\int \frac{\tau(t) = \sigma \left(\mu^* + a \ln \frac{V}{V^*} + b \ln \frac{\theta V^*}{D_c}\right)}{\frac{d\theta}{dt} = 1 - \frac{\theta V^*}{D_c}}$$

Stick-slip requires rateweakening friction a-b < 0



Rate&State Friction Model





The 2011, M_w9.0 Tohoku-Oki Earthquake



Source model determined from the joint inversion of CGPS, teleseismic and acclereometric records (Wei et al., EPSL, 2012)





Co-, Post- and Inter-seismic Models of the 2011 M_w9.0 Tohoku-Oki Earthquake





Method: Joint inversion of onshore GPS time series and offshore campaign data for co- and post-seismic slip using **PCAIM** (Kosistsky and Avouac, 2010) **Data:** GEONET+ seabottom data (Inuma et al, JGR, 2012)



Co-, Post- and Inter-seismic Models of the 2011 M_w9.0 Tohoku-Oki Earthquake

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Co-, Post- and Inter-seismic Models of the 2011 M_w9.0 Tohoku-Oki Earthquake

Interseismic Coupling





- Data: Interseismic GPS velocities from GEONET (Loveless and Meade, 2010,2011)
 - Sea bottom displacements (Matsumoto et al. EPS, 2008)

Implication

 Return Period of Tohoku Oki EQ estimate to 100yr (BT) - 300yr (FT)

Dynamic Modeling

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Thermal Pressurization allows overlapping seismic and aseismic slip (Noda and Lapusta, 2012)



Dynamic Modeling



Rupture propagation



Dynamic modeling

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Numerical Method: Boundary Intregral Method in 3-D (Lapusta and Liu (JGR, 2009)

(Kaneko, Avouac and Lapusta, 2010)



Interseismic coupling

Partial Coupling:

In kinematic inversions ISC is allowed to vary between 0 and 1.

Implication:

Seismic slip is required to balance the quantity ISC x Long Term Slip Rate





Interseismic coupling

Partial Coupling:

In kinematic inversions ISC is allowed to vary between 0 and 1.

Implication:

Seismic slip is required to balance the quantity ISC x Long Term Slip Rate Compared to the case ISC=1, ISC=0.5 requires transients slip events half as large, or a return period twice as long.









(Nadaya Cubas et al, T22C-08.)

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Interseismic coupling





(Kaneko, Avouac and Lapusta, 2010)





Correlation of ISC with seismicity



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